## Low EMI power design ADI Silent Swither products

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## We solve the Three Key Power Supply

## Performance Metrics Form Factor, Efficiency, EMI

## Power Innovation Technologies



The Problem in Traditional Synchronous Buck Converters High di/dt Currents in SMPS Hot Loops Create EMI

Parasitic inductance due to copper traces, bond wires, ESL of capacitors and FET internal metal


Excessive rings at the switching edges cause conductive noise and radiation


## Minimizing Hot Loop

- With monolithic switcher, the best way is to place the low ESL input capacitor as close to the $\mathrm{V}_{\mathbb{I N}}$ and GND as possible
- A solid GND plane with minimum distance to the hot loop is one of the most effective ways to reduce EMI


LARGE EMil BURST! Occurs every switching cycle!


## Silent Swither 1

## Innovation - Silent Switcher



## Silent Switcher 1

## 5V 5A Step-Down Converter



## Silent Switcher Eliminates Switch Ringing

## Silicon Die



LT8610: Wirebonded in MS16E

LT8614: Silent Switcher 1: Magnetic cancellation + CuPillar Flip-Chip

## Silent Switcher Platform - Innovations To Deal with Hot Loop

- Buck regulator platform
- 20dB EMI improvement - No compromise in efficiency and size!
- Offers customers:
- High frequency
- High efficiency
- High current
- Low EMI noise
- Solder joint reliability
- Technologies
- Circuits
- Process/devices
- Package

5V 4A Step-Down Converter


- In-package passive


Figure 2. LT8610 and LT8614 700kHz 14 V to 3.3V 2A Radiated EMI in GTEM Corrected for OATS

## Silent Swither 2

## Silent Switcher 2:

Flip chip on laminate (FCOL) and Cap-In-Package


## Imporve Performance




1ns/DIV

## Silent Switcher 2 Example Excellent EMI Test Results





## A Paradigm Shift <br> Fast Switching Enables Ultralow EMI and High Efficiency

No slew rate limit on switching node necessary to achieve low EMI!


- Hot loop area and inductance virtually zero
- Extremely fast switching
- Neglectable overshoot and no parasitic oscillation on switching node
- Dead time only 1 ns


## Unmatched switching performance!

- Silent Switcher ${ }^{\circledR} 2$ architecture
- Internal bypass capacitors reduce radiated EMI
- Optional spread spectrum modulation
- Ultralow EMI on any PCB, eliminate PCB layout sensitivity
- Wide input range: 3.0V to 42V



5V/4A, 3.3V/4A 2MHz Step-Down Converter


## Silent Switcher 2 Platform

- Buck Regulator Platform
- Offers to the customer:
- High Frequency
- High Efficiency
- High Current
- Low EMI Noise
- Solder Joint Reliability
- Tech:
- Circuits
- Process/Devices
- Package

- In-Package Passives


## LT8650S Passes EMI Tests

Conducted EMI Performance


Radiated EMII Performance (CISPR25 Radiated Emission Test with Class 5 Peak Limits)


## Silent Switcher Family

| DEVICE | \# OF OUTPUTS | $\mathrm{V}_{\text {IN }}$ RANGE | OUTPUT CURRENT | PEAK EFFICEINCY AT 2MHz, 12 V TO 5 V |  | FEATURES | PACKAGES |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LT8650S | 2 | 3V-42V | $4 A+4 A$ on both channels or 6 A on either channel | 94.60\% | $6.2 \mu \mathrm{~A}$ | Silent Switcher 2 | $6 \mathrm{~mm} \times 4 \mathrm{~mm} \times 0.95 \mathrm{~mm}$ <br> LQFN |
| LT8645S | 1 | $3.4 \mathrm{~V}-65 \mathrm{~V}$ | 8A | 94\% | $2.5 \mu \mathrm{~A}$ | Silent Switcher 2 | $6 \mathrm{~mm} \times 4 \mathrm{~mm} \times 0.95 \mathrm{~mm}$ LQFN |
| LT8643S | 1 | $3.4 \mathrm{~V}-42 \mathrm{~V}$ | 6A continuous 7A peak | 95\% | $120 \mu \mathrm{~A}$ | Silent Switcher 2, external compensation | $\begin{aligned} & 4 \mathrm{~mm} \times 4 \mathrm{~mm} \times 0.94 \mathrm{~mm} \\ & \text { LQFN } \end{aligned}$ |
| LT8640S | 1 | $3.4 \mathrm{~V}-42 \mathrm{~V}$ | 6A continuous 7A peak | 95\% | $2.5 \mu \mathrm{~A}$ | Silent Switcher 2 | $4 \mathrm{~mm} \times 4 \mathrm{~mm} \times 0.94 \mathrm{~mm}$ <br> LQFN |
| LT8609S | 1 | $3 \mathrm{~V}-42 \mathrm{~V}$ | 2 A continuous 3 A peak | 93\% | $2.5 \mu \mathrm{~A}$ | Silent Switcher 2 | $3 \mathrm{~mm} \times 3 \mathrm{~mm} \times 0.94 \mathrm{~mm}$ <br> LQFN |
| $\begin{aligned} & \text { LT8640 } \\ & \text { LT8640-1 } \end{aligned}$ | 1 | $3.4 \mathrm{~V}-42 \mathrm{~V}$ | 5A continuous 7A peak | 95\% | $2.5 \mu \mathrm{~A}$ | Silent Switcher, LT8640 pulse skipping, LT8640-1 forced continuous | $3 \mathrm{~mm} \times 4 \mathrm{~mm}$ QFN-18 |
| LT8641 | 1 | $3 \mathrm{~V}-65 \mathrm{~V}$ | 3.5A continuous 5A peak | 94\% | $2.5 \mu \mathrm{~A}$ | Silent Switcher | $3 \mathrm{~mm} \times 4 \mathrm{~mm}$ QFN-18 |
| LT8614 | 1 | $3.4 \mathrm{~V}-42 \mathrm{~V}$ | 4A | 94\% | $2.5 \mu \mathrm{~A}$ | Silent Switcher. Low ripple Burst Mode operation | $3 \mathrm{~mm} \times 4 \mathrm{~mm}$ QFN-18 |

Package technology improves performance, options for customer

| LT8610 | LT8640 | LT8640S |
| :---: | :---: | :---: |
| MSOP-16 | MSOP-16 | MSOP-16 |
|  |  | (BT laminate LGA) |

LTM8053 $6 \times 9$ BGA


## 40Vin Step-Down $\mu$ Module Regulator Size Comparison



## 40Vin Silent Switcher $\mu$ Module Regulators

|  | LTM8074 | LTM8063 | LTM8065 | LTM8053 |
| :---: | :---: | :---: | :---: | :---: |
| Silent Switcher | Yes |  |  |  |
| CISPR22 Class B Compliant | Yes |  |  |  |
| Vin Range | 3.2 V to 40V | 3.2 V to 40V | 3.4 V to 40V | 3.4 V to 40V |
| Vout Range | 0.8 V to 12 V | 0.8 V to 15 V | 0.97 V to 15 V | 0.97 V to 15V |
| Iout | 1.2A (Continuous) 1.75A (Peak) | 2A (Continuous) <br> 2.5A (Peak) | 2.5A (Continuous) 3.5A (Peak) | 3.5A (Continuous) 6A (Peak) |
| Switching Frequency |  | 200 kHz to 2.2 MHz | 200 kHz to 3 MHz | 200 kHz to 3 MHz |
| Package Size (mm) | $4 \times 4 \times 2.22$ | $4 \times 6.25 \times 2.22$ | $6.25 \times 6.25 \times 2.32$ | $6.25 \times 9 \times 3.32$ |
| Package Type | BGA | BGA | BGA | BGA |
| RPL Schedule | Q3 CY2018 | Released |  |  |

## Application

## Improve System performance

## Silent Switcher Application



## Silent Switcher Application



## Silent Switcher Application

| AD9625-2.6 GHz Dynamic Performance |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input <br> Frequency <br> (MHz) | SNRFS (db) <br> Baseline Power <br> Supply |  |  |  | LTM8065 <br> Version1 | LTM8065 <br> Version 2 |
|  | 57.01 | 57.03 | 57.01 | Baseline Power <br> Supply | LTM8065 <br> Version1 | LTM8065 <br> Version2 |
|  | 56.53 | 56.49 | 56.54 | 78.41 | 79.72 | 80.11 |

AD9625 FFT using LTM8065 (AIN $=1349 \mathrm{MHz}$ )


AD9625 FFT using LTM8065 + LC Filter (AIN $=1349 \mathrm{MHz}$ )


| Baseline Power Supply |  | Voltage (V) | Current (A) | Power (W) |
| :---: | :---: | :---: | :---: | :---: |
|  | PIN | 11.729 | 0.676 | 7.929 |
|  | AVDD_1.3V | 1.268 | 1.222 | 1.549 |
|  | DRVDD_1.3V | 1.301 | 0.521 | 0.678 |
| P | DVDD_1.3V | 1.305 | 0.406 | 0.530 |
| 0 | AVDD_2.5V | 2.589 | 0.408 | 1.056 |
| U | DRVDD_2.5V | 2.590 | 0.0047 | 0.012 |
| T | DVDD_2.5V | 2.590 | 0.0001 | 0.0003 |
|  | DVDDIO_3.3V | 3.301 | $0.00 \cap 4$ | 0.0013 |
|  |  |  | POUT TOTAL: | 3.827 |
|  |  |  | Efficiency (\%): | 48.26 |


| LTM8065 Version 2 | Voltage (V) | Current (A) | Power (W) |
| :--- | :--- | :--- | :--- |



## Silent Switcher Application

EVAL-AD9625 Evaluation Board


REVISED Evaluation Board USING LTM8065 POWER SOLUTION



## Test Guaranteed VS Design Guaranteed

## - Low $20 \mu \mathrm{~A}$ Quiescent Current

- +3.5 V to +30 V Wide Input Voltage Range, +45 V Tolerant
- Operates Through Cold-Crank Conditions
- Low-Dropout Voltage of 280 mV at 200 mA
- Up to 200mA Output Current Capability
- Stable Operation with Tiny $4.7 \mu$ F Output Capacitor
- User$\begin{array}{cc}\text { ser- } \\ +3 . & 200 \text { A. AUtOMOtIVE } \\ +1 . & \text { Quİ } \\ \text { Rescent Currenty }\end{array}$
- Open
- Fixed
- High-
- Thern
- Opera
- Autor


## ELECTRICAL CHARACTERISTICS (1

## otherwise note

 Typical values are $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.) (Note 2)| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SETOV INPUT (TRI-MODE) |  |  |  |  |  |  |
| SETOV Input Leakage Current |  | $\begin{aligned} & \text { SET }=\text { HIGH, VSETOV }=5 \mathrm{~V} \\ & \text { or SET }=\text { GND, VSETOV }=5 \mathrm{~V} \end{aligned}$ |  | 1 |  | $\mu \mathrm{A}$ |
| SETOV Low-Level Input Voltage | VILSETOV | SET $=$ GND, VSETOV $<$ VILSETOV or places device in +3.3 V fixed output-voltage mode |  |  | 0.4 | V |
| SETOV High-Level Input Voltage | VIHSETOV | SET $=$ GND, VSETOV $>$ VIHSETOV or places device in +5 V fixed outnut-voltace mode | $\begin{aligned} & \text { Vout } \\ & -0.4 \end{aligned}$ |  |  | V |

Note 2: Production tested at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$. Overtemperature limits are guaranteed by design.

## Design Tools: Step-by-Step Power Supply Design



Enter specs,
search solution.


Power Supply
Schematic.


Efficiency \& Power Loss


Loop Stability \& Transient


LTspice


